## On Computational Complexity of Vortex Element Method for 2D Incompressible Flows Simulation

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## FSI coupled problems

- Movable bodies
- Deformable bodies

Variable flow region angle

How to construct mesh? How to satisfy BC?

## Main assumptions

- 2D flows are considered
- Flow is viscous incompressible
- Airfoils are heavy  $(\rho_0/\rho \gg 1)$  $\rho_0$  — airfoil's average density  $\rho$  — density of the flow



## On the Development of Vortex Methods

## Scientific schools

- S.M. Belotserkovskii, M.I. Nisht, I.K. Lifanov, A.V. Setukha (Zhukovsky Air Force Engineering Academy, MSU);
- S.V. Guvernyuk, G.Ya. Dynnikova (MSU);
- V.I. Morozov, V.A. Aparinov (Scientific and research inst. of parachute design and prod.);
- M.A. Golovkin, V.M. Kalyavkin (Central Aerohydrodynamic Institute);
- G.A. Shcheglov, I.K. Marchevsky (BMSTU);
- D.N. Gorelov (Siberian Branch of the Russian Academy of Sciences, Tomsk);
- S.A. Dovgiy, D.I. Cherniy (National Academy of Sciences of Ukraine, Kiev);
- A. Leonard, G. Winckelmans (Belgium);
- G H. Cottet, P. Koumoutsakos (France, Switzerland);
- G. Morgenthal (Great Britain).

#### Conferences on Vortex Methods

- International conference on vortex flows and models (2010, 2016);
- International conference 'Coupled Problems' (ECCOMAS) (2013, 2015);
- International symposium 'Method of discrete singularities in math. physics' (2003 2013);
- International seminar named after S.M. Belotserkovskii (2004 2015);

## Features of Vortex Method

- Lagrangian meshless method (Particle method);
- easy to solve coupled FSI problems;
- small numerical viscosity;
- possibility to obtain acceptable results for practical problems with small computational burden;
- application area of vortex method:
  - airframe and parachute engineering;
  - aircraft vortex wake calculation;
  - modeling of the main and tail helicopter rotors;
  - industrial aerodynamics of buildings, urban aeration.

#### Disadvantages of vortex method

- application area: incompressible flow;
- law accuracy of vortex sheet computation;
- need to consider pair influences for all vortex elements (as in N-body problem).

## Equations of fluid motion and boundary conditions

**Continuity & Navier — Stokes equations:** 

$$abla \cdot ec{V} = \mathbf{0}, \qquad rac{\partial ec{V}}{\partial t} + (ec{V} \cdot 
abla) ec{V} = 
u \Delta ec{V} - rac{
abla p}{
ho}.$$

#### **Boundary conditions:**



Conditions of perturbations decay at infinity:

$$ec{V}(ec{r},t)
ightarrow ec{V}_{\infty}, \quad p(ec{r},t)
ightarrow p_{\infty}, \quad |ec{r}|
ightarrow \infty.$$

No-slip condition:  $\vec{V}(\vec{r},t) = \vec{V}_{K}(\vec{r},t), \quad \vec{r} \in K.$ 

 $\vec{V}$  - velocity in the flow;  $\vec{V}_{\infty}$ ,  $p_{\infty}$  - velocity and pressure at infinity; p - pressure;  $\nu$  - kinematic viscosity coefficient.

## Basic Ideas

## Viscous Vortex Domains (VVD) method

- Vorticity  $\vec{\Omega}(\vec{r},t) = 
  abla imes \vec{V}(\vec{r},t)$  primary compute variable.
- Navier Stokes equations in Helmholtz form:

$$\frac{\partial \vec{\Omega}}{\partial t} + \nabla \times \left( \vec{\Omega} \times (\vec{V} + \vec{W}) \right) = 0.$$

• It can be treated as transport equation for  $\vec{\Omega}$ , which moves in velocity field  $\vec{V} + \vec{W}$ ,

$$ec{W}(ec{r},t)=-
urac{
abla\Omega}{\Omega}-$$
 diffusive velocity,  $\Omega=ec{\Omega}\cdotec{k}.$ 

- No vorticity generation in flow region.
- New vorticity is generated only on the camber line of the airfoil.
- 1. Dynnikova, G.Ya. The Lagrangian approach to solving the time-dependent Navier Stokes equations. *Doklady Physics*. (2004) **49**: 648–652.

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#### Vortex and source Sheets

Airfoil influence is simulated by attached vortex and source sheets and free vortex sheet placed on its camber line:

• Intensity of the attached vortex sheet

$$\gamma_{\mathsf{att}}(\vec{r}, t) = \vec{V}_{\mathcal{K}}(\vec{r}, t) \cdot \vec{\tau}(\vec{r}, t), \quad \vec{r} \in \mathcal{K}.$$

• Intensity of the attached source sheet

$$q_{\mathrm{att}}(\vec{r}, t) = \vec{V}_{\mathcal{K}}(\vec{r}, t) \cdot \vec{n}(\vec{r}, t), \quad \vec{r} \in \mathcal{K}.$$

• Intensity of the free vortex sheet  $\gamma(\vec{r}, t)$  can be determined from the boundary condition satisfaction.

 $\vec{\tau}(\vec{r}, t)$  и  $\vec{n}(\vec{r}, t)$  — unit normal and tangent vectors.

## Flow Velocity

#### Generalized Biot — Savart law

$$\begin{split} \vec{V}(\vec{r},t) &= \vec{V}_{\infty} + \frac{1}{2\pi} \int_{S(t)} \frac{\vec{\Omega}(\vec{\xi},t) \times (\vec{r}-\vec{\xi})}{|\vec{r}-\vec{\xi}|^2} dS + \frac{1}{2\pi} \oint_{K(t)} \frac{\vec{\gamma}(\vec{\xi},t) \times (\vec{r}-\vec{\xi})}{|\vec{r}-\vec{\xi}|^2} dI_K + \\ &+ \frac{1}{2\pi} \oint_{K(t)} \frac{\vec{\gamma}_{\mathsf{att}}(\vec{\xi},t) \times (\vec{r}-\vec{\xi})}{|\vec{r}-\vec{\xi}|^2} dI_K + \frac{1}{2\pi} \oint_{K(t)} \frac{q_{\mathsf{att}}(\vec{\xi},t)(\vec{r}-\vec{\xi})}{|\vec{r}-\vec{\xi}|^2} dI_K, \\ \vec{\gamma}_{\mathsf{att}} &= \gamma_{\mathsf{att}} \vec{k}, \qquad \vec{\gamma} = \gamma \vec{k}, \qquad \vec{\Omega} = \Omega \vec{k}, \qquad \vec{n}(\vec{r},t) \times \vec{\tau}(\vec{r},t) = \vec{k}. \end{split}$$

Limit value of the velocity on the airfoil camber line

$$ec{V}_{-}(ec{r},\,t) = ec{V}(ec{r},\,t) - rac{\gamma(ec{r},\,t) - \gamma_{
m att}(ec{r},\,t)}{2} ec{ au}(ec{r},\,t) + rac{q_{
m att}(ec{r},\,t)}{2} ec{n}(ec{r},\,t)$$

- 1. Zhukovsky N.E. On attached vortices. 1908.
- Kempka S.N., Glass M.W., Peery J.S., Strickland J.H. Accuracy considerations for implementing velocity boundary conditions in vorticity formulations // SANDIA REPORT. SAND96-0583, UC-700, 1996. 52 p.

## Numerical Approximation

### Vortex wake simulation

Vorticity distribution in the flow is simulated by large number of separate vortex elements (VE) (VE)

$$\Omega(\vec{r}) = \sum_{i=1}^{n} \Gamma_i \delta(\vec{r} - \vec{r}_i),$$

 $\Gamma_i$  — circulation of the  $\overline{VEs}$ ,  $\vec{r_i}$  — their positions.



#### Vortex elements movement

ent equation: 
$$\frac{D\vec{\Omega}}{Dt} = 0 \quad \Leftrightarrow \quad \begin{cases} \Gamma_i = \text{const}, \\ \frac{d\vec{r}_i}{dt} = \vec{V}(\vec{r}_i) + \vec{W}(\vec{r}_i), \quad i = 1, \dots, n. \end{cases}$$

$$ec{V}(ec{r}_i) = \sum_{\substack{j=1\ j 
eq i}}^n \underbrace{rac{\Gamma_j}{2\pi} rac{ec{k} imes (ec{r}_i - ec{r}_j)}{|ec{r}_i - ec{r}_j|^2}}_{ec{v}_{ij}} + ec{V}_\gamma + ec{V}_\gamma^{ ext{att}} + ec{V}_q^{ ext{att}} + ec{V}_\infty.$$

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Movem

## Free Vortex Sheet Intensity Computation

#### No-slip boundary condition



T-scheme Kempka, S.N., Glass, M.W., Peery, J.S. and Strickland J.H. Accuracy Considerations

for Implementing Velocity Boundary Conditions in Vorticity Formulations. SANDIA Report SAND96-0583, 1996.

Cottet G.-H., Koumoutsakos P.D. Vortex Methods: Theory and Practice. — Cambridge University Press, 2008. — 328 p.

#### T-scheme allows to obtain much more accurate results when solving FSI-problems

- 1. Marchevsky, I.K. and Moreva, V.S. Vortex Element Method for 2D Flow Simulation with Tangent Velocity Components on Airfoil Surface. *ECCOMAS 2012 European Congr. on Comp. Meth. in Appl. Sc. and Eng., e-Book.* (2012) 5952–5965.
- Kuzmina K.S., Marchevsky I.K. The Modified Numerical Scheme for 2D Flow-Structure Interaction Simulation Using Meshless Vortex Element Method // PARTICLES 2015: Proc. of the IV Inter. Conf. on Particle-Based Methods (Barcelona, Spain, 28 – 30 Sept. 2015). – 2015. Pp. 680–691.

# Comparison of N- and T-scheme accuracy for flow simulation around elliptical airfoil



## Comparison of *N*- and *T*-scheme accuracy for flow simulation around Zhukovsky airfoil



• a = 3.5, d = 0.4, h = 0.3 -

## Goal

The estimation of computational complexity of the vortex method and its effective implementation.

## Objectives

- 'Typical' model problems statement.
- Analysis of the computational complexity of the main algorithm operations.
- Analysis of the possible ways to accelerate calculations.
- Optimized algorithm complexity estimation.
- Model problems solving.

## Model problems description. Problem 1

### Simulation of hydroelastic oscillations of two cylinders

#### 'Base' parameters of numerical scheme:

•  $\mathbf{n_{p0}}=200-$  number of vortex elements that simulate vortex sheet on one cylinder;

 $\mathbf{n}_0 = 2 \cdot n_{p0} = 400$  — total number of vortex elements that simulate vortex sheet.

•  $N_{p0} = 10\,000$  — number of vortex elements that simulate vortex wake near one cylinder;

 $N_0 = 20\,000$  total number of vortex elements that simulate vortex wake.

•  $T_0 = 30000$  — number of required time steps.



## Model problems description. Problem 2

## Simulation of hydroelastic oscillations of cylinder in presence of shielding surface

Vortex layer on the shielding surface remains to be attached.



## 'Base' parameters of numerical scheme:

 $\mathbf{n_{p0}} = 200 \text{ VE} - \text{vortex sheet on}$  the cylinder;

 $\mathbf{n_{e0}} = 3n_{p0} = 600 \text{ VE} - \text{vortex}$ sheet on the shielding surface;  $\mathbf{N_0} = 10\,000 \text{ VE} - \text{vortex wake}.$ 

### Parameters for arbitrary $n_p$

$$n = 4n_p$$
,  $N = N_0 \cdot \left(\frac{n_p}{n_{po}}\right)^2$ ,  $T = T_0 \cdot \left(\frac{n_p}{n_{p0}}\right)$ .

## Computational complexity for main operations

• **Operation 1.** SLAE matrix formation for generated vortex elements circulations determination.

 $\label{eq:Q1} \begin{array}{ll} Q_1^{\sf N}=6n^2, & Q_1^{\sf T}=83n^2.\\ \bullet \mbox{ Operation 2. SLAE right hand side calculation.} \\ & Q_2^{\sf N}=7Nn+10n^2, & Q_2^{\sf T}=30Nn+85n^2. \end{array}$ 

• **Operation 3.** SLAE solving or multiplying by inverse matrix.

$$Q_3=n^3/3 \quad \text{ or } \quad Q_3=n^2.$$

- Operation 4. Calculation of convective velocities of vortex elements.  $Q_4 = 6 N^2 + 8 N n. \label{eq:Q4}$
- **Operation 5.** Calculation of diffusive velocities of vortex elements.

$$\mathbf{Q}_5 = \mathbf{9N^2} + \mathbf{14Nn}.$$

• **Operation 6.** No-through control block.

$$\mathbf{Q_6} pprox \mathbf{Q_1}$$

• Operation 7. Vortex wake reconstruction.

 $Q_7\approx 0{,}2Q_4.$ 

$$Q = \frac{n^3}{3} + 251 \, n^2 + 53,\! 6 \, N \, n + 16,\! 2 \, N^2. \label{eq:Q}$$

## Operations $Q_1 \dots Q_7 \; (\%)^{\dagger}$





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## Total numerical complexity of model problems

$$S_1(200) = Q_1(200) \cdot T_0 \approx 2, 1 \cdot 10^{14},$$

$$S_2(200) = Q_2(200) \cdot T_0 \approx 7, 1 \cdot 10^{13}$$

Пр	100	200	400	600	800	1000
$\frac{S_1(n_p)}{S_1(200)}$	0,03	1	31	231	969	2946
$\frac{S_2(n_p)}{S_2(200)}$	0,05	1	26	188	766	2293

#### Ways to accelerate computations

- Use parallel computing.
- Use approximate fast methods:
  - fast multipole method;
  - mosaic-skeleton approximations (E.E. Tyrtyshnikov);
  - auxiliary Poisson equation solving.

# Usage of parallel computing technologies for vortex method implementation

### 'Old' implementation

In [\*] algorithm with parallel implementation of operations 4, 5, 6, 7 was described.

<u>1 problem</u>. Speeding up 25-30 times in the calculations on the 64-core cluster. Amdahl law predicts 45 times acceleration.

<u>2 problem</u>. Speeding up 5 times in the calculations on the 64-core cluster. Amdahl law predicts 7.5 times acceleration.

Parallel implementation of 4 operations is not enough! It is necessary to develop parallel algorithms for all seven major operations of vortex method!

[\*] Марчевский И.К., Морева В.С. Параллельный программный комплекс POLARA для моделирования обтекания профилей и исследования расчетных схем метода вихревых элементов // Параллельные вычислительные технологии (ПаBT'2012): Труды международной научной конференции (Новосибирск, 26–30 марта 2012 г.). Челябинск: Издательский центр ЮУрГУ, 2012. С. 236–247.

## Acceleration with 'old' parallel implementation



## Fast method (by analogy with *N*-body problem)

Barnes J., Hut P. A hierarchical O(N log N) force-calculation algorithm // Nature. 1986. V. 324, No. 4. P. 446-449.



- Collective influence of remote VE is calculated approximately.
- The basis of the algorithm creation of the hierarchical tree structure.



Tree structure and traversal scheme



Velocities of all vortex elements in considered cell of lower level

$$ec{V}_i pprox egin{pmatrix} A \ B \end{pmatrix} + egin{pmatrix} C & D \ D & -C \end{pmatrix} egin{pmatrix} \Delta x_i \ \Delta y_i \end{pmatrix} + \sum_i ec{v}_{ij} + ec{V}_\infty$$

A, B, C  $\mu$  D — calculated coefficients, which are common for all VE in cell.

#### Algorithm parameters

•  $\theta$  — cells proximity parameter ( $0 \le \theta \le 4$ ), determined by required accuracy. Proximity condition:  $|\vec{r}'| \le \frac{h+h_0}{\theta}$ .

• k — maximal tree level.

## Computational complexity

Direct calculation	Fast method	
$O(N^{2})$	$O(N \log N)$	
	with optimal <i>k</i>	

# Approximate estimation of computational complexity of fast algorithm

Number of multiplications and divisions in convective velocities computation using fast method  $(Q_4)$ 

$$\begin{aligned} Q_4^{fast} &= \frac{24N^2}{2^k} \left(\frac{4}{\theta}\right)^2 \left(1 - \alpha \frac{(\sqrt{2})^k - 1}{\sqrt{N}}\right)^2 \left(1 - \frac{4}{\theta(\sqrt{2})^k} \left(1 - \alpha \frac{(\sqrt{2})^k - 1}{\sqrt{N}}\right)\right) + \\ &+ \frac{896 \cdot 2^k \cdot \beta}{\theta^2} \left(4 \left(\frac{1}{4+\theta} + \frac{1}{4-(\sqrt{2})^k \theta}\right) + \ln\left(\frac{(\sqrt{2})^k - 4}{4+\theta}\right)\right) + 4N. \end{aligned}$$

N — number of VE in flow region,  $\alpha$ ,  $\beta$  — experimentally selected parameters ( $\alpha = 0.84$ ,  $\beta = 0.56$ ).  $\theta \approx 0.4$  gives  $0, 1 \dots, 0, 2$  % error.

Кузьмина К.С., Марчевский И.К. Оценка трудоемкости быстрого метода расчета вихревого влияния в методе вихревых элементов // Наука и образование: электронное научно-техническое издание. 2013. № 10. С. 399-414.

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#### Diffusive velocities computation using fast method $(Q_5)$

$$Q_5 = \left. Q_4 \right|_{\theta = heta_{dif}} \cdot N \cdot heta_{dif} \cdot rac{\gamma}{2^k}.$$

 $\gamma = 0,7$  — empirical coefficient;  $\theta_{dif}$  — parameter which determines the accuracy of method, k — number of layers.  $\theta_{dif} \approx 0,1$  gives  $0,1\ldots,0,2$  % error.

### SLAE right-hand side calculation $(Q_2)$

$$Q_{2}^{fast} = \frac{130Nn}{2^{k}} \left(\frac{4}{\theta}\right)^{2} \left(1 - \alpha \frac{(\sqrt{2})^{k} - 1}{\sqrt{N}}\right)^{2} \left(1 - \frac{4}{\theta(\sqrt{2})^{k}} \left(1 - \alpha \frac{(\sqrt{2})^{k} - 1}{\sqrt{N}}\right)\right) + \frac{896 \cdot n \cdot \beta}{\theta^{2}} \left(4 \left(\frac{1}{4 + \theta} + \frac{1}{4 - (\sqrt{2})^{k}\theta}\right) + \ln\left(\frac{(\sqrt{2})^{k} - 4}{4 + \theta}\right)\right) + 85n^{2}.$$

Кузьмина К.С., Марчевский И.К. Об оценках вычислительной сложности и погрешности быстрого алгоритма в методе вихревых элементов // Труды Института системного программирования РАН. 2016. Т. 28. № 1. В печати.

## Acceleration of operations $Q_2$ , $Q_4$ , $Q_5$ using fast method





#### Other operations of algorithm

Operations 6 (no-through control) and 7 (vortex wake reconstruction) also can be accelerated using tree structure:

$$Q_6^{fast} = Q_1^{fast}, \qquad Q_7^{fast} = 0.2Q_4^{fast}.$$

Operations 1 (SLAE matrix formation) and 3 (SLAE solving) cannot be accelerated using fast method:

$$Q_1^{fast} = Q_1, \qquad Q_3^{fast} = Q_3.$$

Computational complexity S (direct calculation) with respect to  $S^{fast}$  (using fast method)



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## Operations $Q_1 \ldots Q_7$ (%) when using fast method





## 'New' algorithm implementation

- 1, 2 and 6 operations parallelized using MPI technology.
- **3 operation** implemented using Eigen library (linear algebra library) using OpenMP.
- For **4 and 5 operations** fast algorithms are implemented, which parallelized using MPI.
- For **7 operation** effective algorithm are implemented using tree structure and MPI technology.

### Problem 1



### Problem 2



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## Conclusions

- It is shown that computational complexity distribution over the operations depend heavily on problem statement.
- The computational complexity estimations of the fast algorithm are obtained; these estimations allow to choose optimal parameters for algorithm.
- Parallel implementation of vortex method using fast method is developed.